

Math Methods in Physics I

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class #21



surface sphere geodesic?

Sphere coordinates Example airplane

$$x = r \sin \theta \cos \phi$$

$$y = r \sin \theta \sin \phi$$

$$z = r \cos \theta$$

$$d\vec{s} = dr\vec{r} + r d\theta\hat{\theta} + r \sin \theta d\phi\hat{\phi}$$

$$ds^2 = dr^2 + r^2 d\theta^2 + r^2 \sin^2 \theta d\phi^2 \quad ds^2 = ds \cdot ds$$

On the sphere, $dr=0$, we $r=1$

$$ds^2 = d\theta^2 + \sin^2 \theta d\phi^2$$

$$\text{Length } L = \int_A^B |ds| = \int_A^B \sqrt{d\theta^2 + \sin^2 \theta d\phi^2}$$

$$\begin{aligned} d\theta^2 + \sin^2 \theta d\phi^2 &= d\theta^2 \left(1 + \sin^2 \theta \frac{d\phi^2}{d\theta^2} \right) \\ &= d\theta^2 \left(1 + \sin^2 \theta \left(\frac{d\phi}{d\theta} \right)^2 \right) \end{aligned}$$

$$\theta = \theta(t) ; \phi(t)$$

$$ds = r \sqrt{\dot{\theta}^2 + \dot{\phi}^2 \sin^2 \theta} dt$$

$$S = \int_A^B \sqrt{\dot{\theta}^2 + \dot{\phi}^2 \sin^2 \theta} dt$$

$$ds^2 = d\theta^2 \left(1 + \sin^2 \theta \left(\frac{d\phi}{d\theta} \right)^2 \right)$$

$$L = \int_A^B |ds| = \int_A^B \sqrt{d\theta^2 + \sin^2 \theta d\phi^2}$$

$$\begin{aligned} d\theta^2 + \sin^2 \theta d\phi^2 &= d\theta^2 \left(1 + \sin^2 \theta \frac{d\phi^2}{d\theta^2} \right) \\ &= d\theta^2 \left(1 + \sin^2 \theta \left(\frac{d\phi}{d\theta} \right)^2 \right) \end{aligned}$$

$$L = \int_A^B |d\theta|$$

$$S = \int |b'(t)| dt = |\theta(b) - \theta(a)|$$

Minimized if and only if $\phi' = 0$. Must lie on a meridian of the sphere $\phi = \phi_0 \equiv \text{const}$. In cartesian,

$$\phi = \tan^{-1} \left(\frac{y}{x} \right) = \phi_0 \equiv \phi_0$$

$$\frac{y}{x} = \tan \phi_0 \quad y \cos \phi_0 = x \sin \phi_0$$

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Path integral

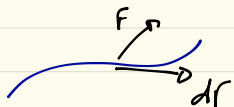
Stokes theorem, Gauss theorem?

Work

$$W = F \cdot d$$

infinitesimal

$$dW = F \cdot dr ; \quad W = \int F \cdot dr$$



$$\text{Given } F = xy\hat{i} - y^2\hat{j}$$

Write the path in terms of a single variable:

Along a straight line $y = \frac{1}{2}x$; $dy = \frac{1}{2}dx$. The limit for x is (0,2):

$$W = \int_0^2 \left[x \left(\frac{x}{2} \right) dx - \left(\frac{1}{2}x \right)^2 \cdot \frac{1}{2} dx \right] = \int_0^2 \frac{3}{8} x^2 dx = \frac{x^3}{8} \Big|_0^2 = 1$$

Along path 2, a parabola

$$y = \frac{1}{4}x^2 ; \quad dy = \frac{1}{2}x dx$$

$$\begin{aligned} W_2 &= \int_0^2 \left(x \cdot \frac{1}{4}x^2 dx - \frac{1}{16}x^4 \cdot \frac{1}{2}x dx \right) = \int_0^2 \left(\frac{1}{4}x^3 - \frac{1}{32}x^5 \right) dx = \\ &= \frac{x^4}{16} - \frac{x^6}{192} \Big|_0^2 = \frac{2}{3} \end{aligned}$$

Along path 3:



$$\int_A^B \mathbf{F} \cdot d\mathbf{r} + \int_B^C \mathbf{F} \cdot d\mathbf{r}$$

$$\int_{y=0}^1 (0 \cdot y \cdot 0 - y^2 dy) = -\frac{y^3}{3} \Big|_0^1 = -\frac{1}{3}$$

$$\int_{x=0}^2 (x \cdot 1 \cdot dx - 1 \cdot 0) = \frac{x^2}{2} \Big|_0^2 = 2$$

$$\text{Then the total } w_3 = -\frac{1}{3} + 2 = \frac{5}{3}$$

Path 4:

$$\text{Parameter } t : x = 2t^3, y = t^2 \quad \therefore dx = 6t^2 dt, dy = 2t dt$$

$$\int_0^1 (2t^3 \cdot t^2 \cdot 6t^2 dt - t^4 \cdot 2t \cdot dt) = \int_0^1 (12t^7 - 2t^5) dt = \frac{12}{8} - \frac{2}{6} = \frac{7}{6}$$

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Conservative Fields

Forces whose work do not depend on the path are called conservative

$$\int_A^B \mathbf{F} \cdot d\mathbf{r} = U(B) - U(A) = \int_A^B dU$$

$$dU = \nabla U \cdot d\mathbf{r} = \frac{\partial U}{\partial x} dx + \frac{\partial U}{\partial y} dy + \frac{\partial U}{\partial z} dz$$

$$\mathbf{F} = \nabla U \quad \therefore \nabla \times \mathbf{F} = \nabla \times \nabla U = 0$$

Conservative fields

Can be written in terms of a potential \Leftrightarrow Have zero curl (irrotational)

Examples: Gravitational force
Electric field (electrostatics).

Gauss theorem and Stokes theorem

Green theorem

$$\int_a^b \frac{d}{dt} f(t) dt = f(b) - f(a)$$

Surface integral over A of $\frac{\partial P}{\partial y}$ is equal to line integral around C .

$$\iint \frac{\partial P}{\partial y} dy dx = \int_a^b dx \int_{y_l}^{y_u} \frac{\partial P}{\partial y} dy = \int_a^b [P(x, y_u) - P(x, y_l)] dx$$

$$= - \int_a^b P(x, y_l) dx - \int_b^a P(x, y_u) dx$$

$$= - \oint P dx$$

$$\therefore \oint_C P dx = - \iint_A \frac{\partial P}{\partial y} dx dy$$

If we did on x first

$$\iint \frac{\partial Q}{\partial x} dx dy = \oint_C Q dy$$

$$\iint_A \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dx dy = \oint_{\partial A} (P dx + Q dy) \quad \partial A = C \text{ (contour of } A \text{)}$$

So, we can say

$$W = \oint_C (F_x dx + F_y dy) = \iint_A \left(\frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y} \right) dx dy$$

$$W = \oint_C \mathbf{F} \cdot d\mathbf{r} = \iint_A (\nabla \times \mathbf{F}) \cdot d\mathbf{A} \quad \text{Show the honeycomb pattern.}$$

P and Q are arbitrary

$$\text{Choose } Q = U_x \text{ and } P = -V_y$$

$$\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} = \frac{\partial U_x}{\partial x} + \frac{\partial V_y}{\partial y} = \nabla \cdot \mathbf{v}$$

$$d\mathbf{r} = dx \hat{i} + dy \hat{j} \text{ (tangent)}$$

Normal? \hat{n}

$$d\mathbf{r} \cdot \hat{n} = 0$$

$$\hat{n} = a \hat{i} + b \hat{j}$$

$$a dx + b dy = 0$$

$$a = dy; b = -dx \quad \therefore \hat{n} = \hat{i} dy - \hat{j} dx$$

So,

$$Pdx + Qdy = -V_y dx + V_x dy = (\hat{i}V_x + \hat{j}V_y) \cdot (\hat{i}dy - \hat{j}dx) \\ = V \cdot \hat{n} ds$$

So, 9.7:

$$\iint \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dx dy = \oint_{\partial A} (Pdx + Qdy)$$

9.9: $\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} = \frac{\partial V_x}{\partial x} + \frac{\partial V_y}{\partial y} = \nabla \cdot V$

$$\iint_A \nabla \cdot V dx dy = \oint_{\partial A} V \cdot \hat{n} ds$$

In 3D

$$\iiint_V \nabla \cdot F dV = \oint_A F \cdot \hat{n} dA$$

For Stokes theorem, define

$$Q = V_y, P = V_x, \text{ with } V = \hat{i}V_x + \hat{j}V_y \quad (9.15)$$

So

$$\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} = \frac{\partial V_y}{\partial x} - \frac{\partial V_x}{\partial y} = (\nabla \times V) \cdot \hat{k}$$

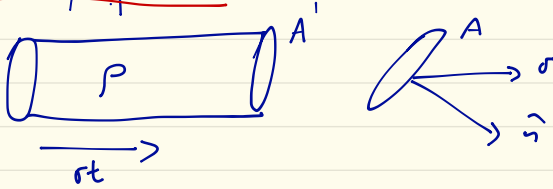
$$9.10 \quad (dr = \hat{i}dx + \hat{j}dy)$$

9.10 and 9.15 yield

$$P dx + Q dy = (\hat{i}V_x + \hat{j}V_y) \cdot (\hat{i}dx + \hat{j}dy) = V \cdot dr$$

$$\iint_A (\nabla \times F) \cdot \hat{n} dA = \oint_{\partial A} F \cdot dr$$

Continuity equation



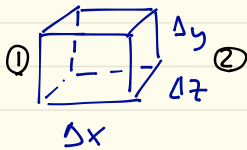
Amount of fluid crossing an area A' in unit time

$$\rho \cdot V = \rho \cdot \vec{v} \cdot t A' = \rho \vec{v} \cdot t A \cos \theta$$

Amount of water crossing a unit area in unit time is

$$\frac{\Delta m}{\Delta t \Delta A} = -\rho \vec{v} \cdot \hat{n}$$

$$\rho \vec{v} = \vec{\phi}$$



Mass entering through ①:

$$\left. \frac{\Delta m}{\Delta t \Delta A} \right|_1 = -\rho \vec{v} \cdot \hat{n} \quad \Big|_1 \quad \frac{\Delta m}{\Delta t} = -\rho \vec{v}_1 \cdot \hat{n} \Delta A_1$$

Mass entering through 2:

$$\frac{\Delta m}{\Delta t} = -\rho \vec{v}_2 \cdot \hat{n} \Delta A_2$$

Net flow:

$$\left(\frac{\Delta m}{\Delta t} \right) \Big|_2 + \left(\frac{\Delta m}{\Delta t} \right) \Big|_1 = \vec{p}_1 \cdot \hat{n} \Delta A_1 + \vec{p}_2 \cdot \hat{n} \Delta A_2$$

$$\Delta A_1 = \Delta A_2 = \Delta y \Delta z$$

$$\begin{aligned} \left(\frac{\Delta m}{\Delta t} \right) \Big|_2 + \left(\frac{\Delta m}{\Delta t} \right) \Big|_1 &= \vec{p}_1 \cdot \hat{n} \Delta A_1 + \vec{p}_2 \cdot \hat{n} \Delta A_2 \\ &= (\vec{p}_2 \cdot \hat{n}_2 + p_1 \hat{n}_1) \Delta y \Delta z \end{aligned}$$

$$\vec{p}_2 \cdot \hat{n}_2 = \vec{p}_2 \cdot (\hat{x}) = p_{x_2} \quad \Rightarrow \quad \vec{p}_1 \cdot \hat{n}_1 = p_1 (-\hat{x}) = -p_{x_1}$$

$$\left(\frac{\Delta m}{\Delta t} \right) \Big|_2 + \left(\frac{\Delta m}{\Delta t} \right) \Big|_1 = (p_{x_2} - p_{x_1}) \Delta y \Delta z = \Delta p_x \Delta y \Delta z$$

$$\text{Take limits now } \lim_{\Delta x \rightarrow 0} \Delta p_x = \lim_{\Delta x \rightarrow 0} \frac{\Delta p_x \Delta x}{\Delta x} = \frac{\partial p_x}{\partial x} dx$$

$$\frac{\partial m}{\partial t} \Big|_2 + \frac{\partial m}{\partial t} \Big|_1 = \frac{\partial p_x}{\partial x} dx dy dz$$

For the other faces of the cube:

$$\frac{\partial m}{\partial t} = \left(\frac{\partial p_x}{\partial x} + \frac{\partial p_y}{\partial y} + \frac{\partial p_z}{\partial z} \right) dx dy dz = \nabla \cdot \vec{p} dV$$

$$\frac{\partial m}{\partial t} = \nabla \cdot \vec{p} \quad \text{Net out-flow per unit volume evaluated at a point.}$$

$$\vec{p} = \rho \cdot \vec{v} \quad m dV = d\rho$$

$$\frac{\partial \rho}{\partial t} = \nabla \cdot (\rho \vec{v})$$

$$\frac{\partial \rho}{\partial t} = \rho \nabla \cdot \vec{v} + (\vec{v} \cdot \nabla) \rho$$

$$\frac{\partial \rho}{\partial t} + (\vec{v} \cdot \nabla) \rho = -\rho \nabla \cdot \vec{v}$$

Mass of fluid going outside

$$\iiint \frac{\partial m}{\partial t} dV = \iint m \vec{v} \cdot \vec{n} dA$$

order of magnitude estimate.

$$\iiint \frac{\partial \rho}{\partial t} dV = \iint \rho \vec{v} \cdot \vec{n} dA$$

$$\iiint \nabla(\rho \vec{v}) dV = \iint \rho \vec{v} \cdot \vec{n} dA$$

Gauss theorem / Divergence theorem

$$\iiint \nabla \cdot \mathbf{F} dV = \iint \mathbf{F} \cdot \mathbf{n} dA$$

Give as example what I did in a paper

$$t_r = \frac{\mathbf{E}}{\mathbf{E}} = \frac{\mathbf{E}}{\nabla \cdot \mathbf{F}} = \frac{\int \mathbf{E} dV}{\int \nabla \cdot \mathbf{F} dV} = \frac{\mathbf{E} \cdot \mathbf{V}}{\mathbf{F} \cdot \mathbf{A}} = \frac{(C_v \rho T) \frac{\pi}{3} H^3}{\frac{\pi}{4} H^2} \sim \frac{C_v \rho H}{3 \sigma T^3}$$

Stokes theorem

Circulation: line integral of vector field

$$\oint \mathbf{F} d\mathbf{r}$$



$$\oint \mathbf{F} \cdot d\mathbf{r} = \iint (\nabla \times \mathbf{F}) \cdot \hat{\mathbf{n}} dx dy = \iint (\nabla \times \mathbf{F}) \cdot \hat{\mathbf{n}} dA$$

Back to green's theorem; \leftarrow

Main application of these theorems is in electrodynamics

$$\oint_C \mathbf{B} \cdot d\mathbf{r} = \mu_0 \iint \mathbf{J} \cdot \mathbf{n} dA$$

Biot-Savart law
to Ampère law

$$\oint (\nabla \times \mathbf{B}) \cdot \mathbf{n} dA \rightarrow \nabla \times \mathbf{B} = \mu_0 \mathbf{J}$$

